

Modeling of Particle Debris from the Target of Laser Produced Plasma EUV Sources

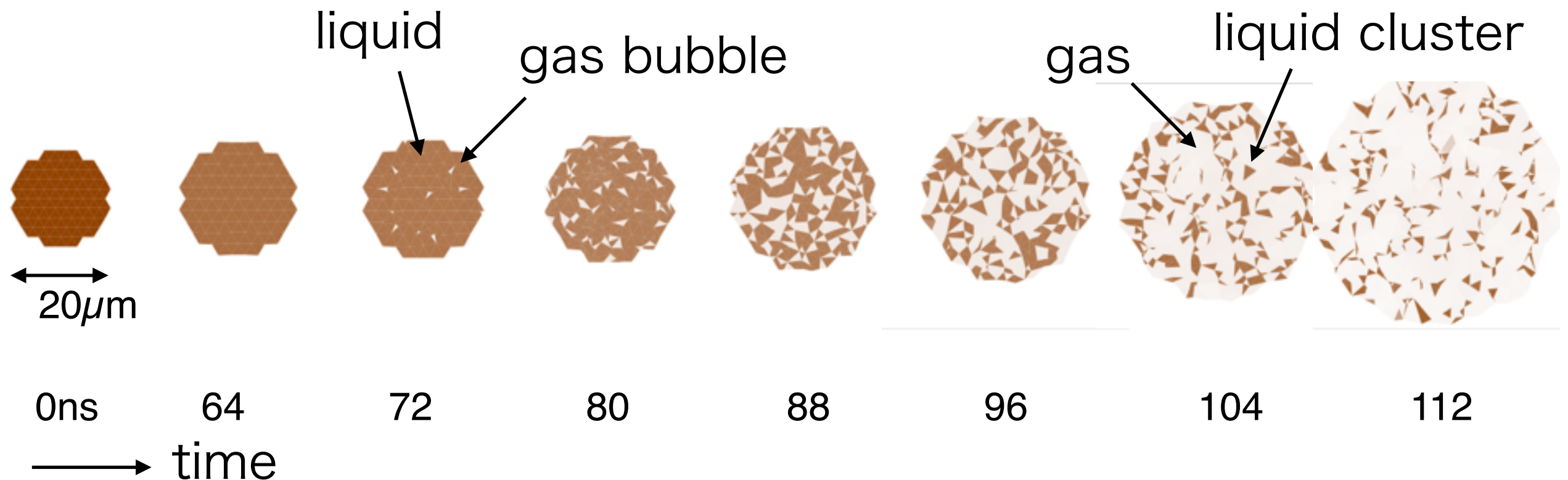
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Emission of particle debris for LPP EUV source

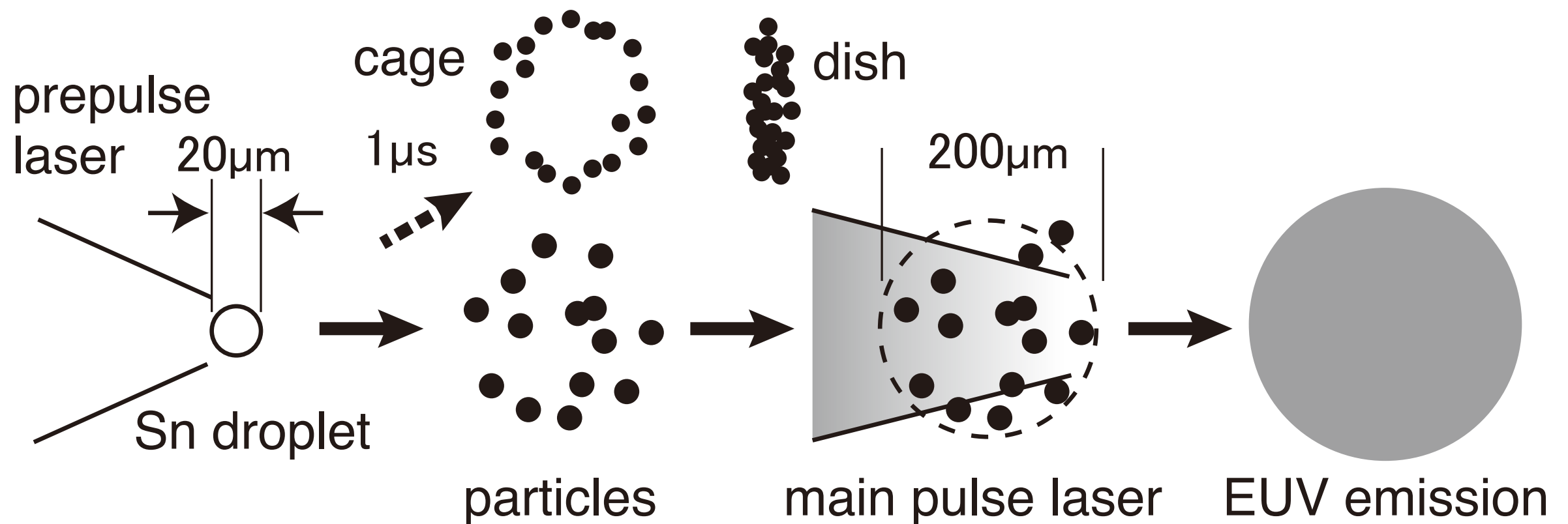
- Particle debris are emitted from laser ablation of Sn droplet.
- Contamination of collector optics limits the availability of the source.
- No simulation is available for the emission of particle debris.

Density profile of uniformly heated droplet

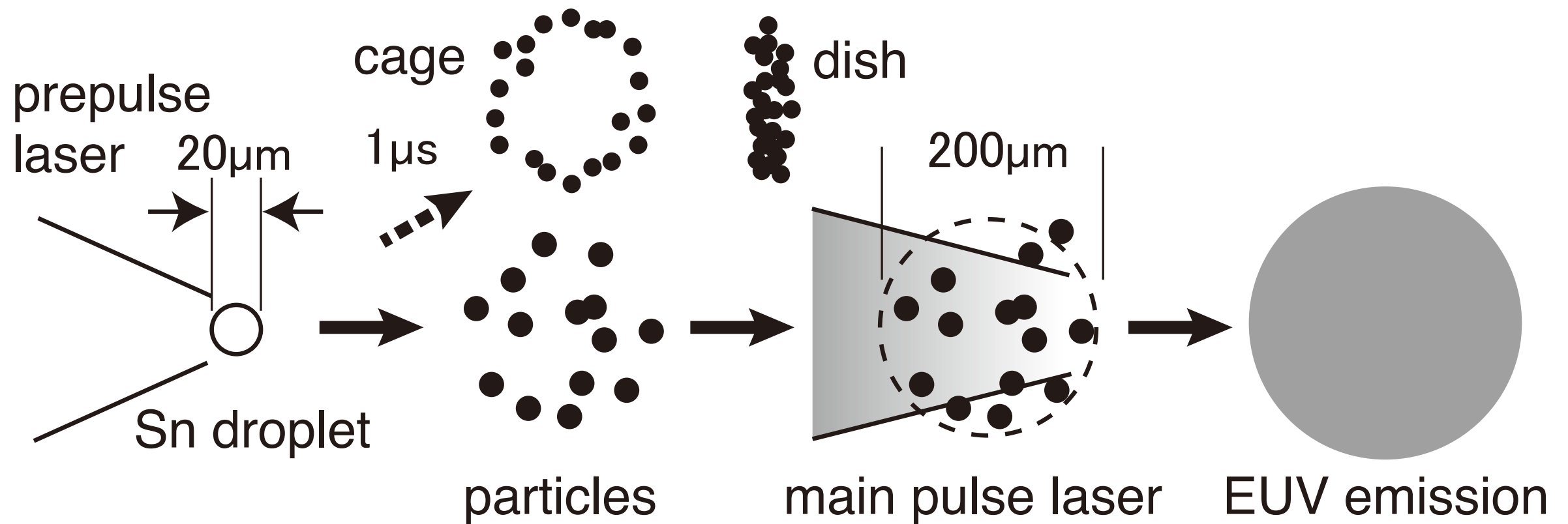


High CE (>5%) using pre-pulse technique

- Droplet is broken up into particles by pre-pulse irradiation.
- Main CO₂ laser pulse irradiates when the cloud of particles expanded to $\approx 200\mu\text{m}$, then plasmas of appropriate density and temperature for emission is produced.
- Laser is absorbed efficiently only with the particles.



High CE (>5%) using pre-pulse technique

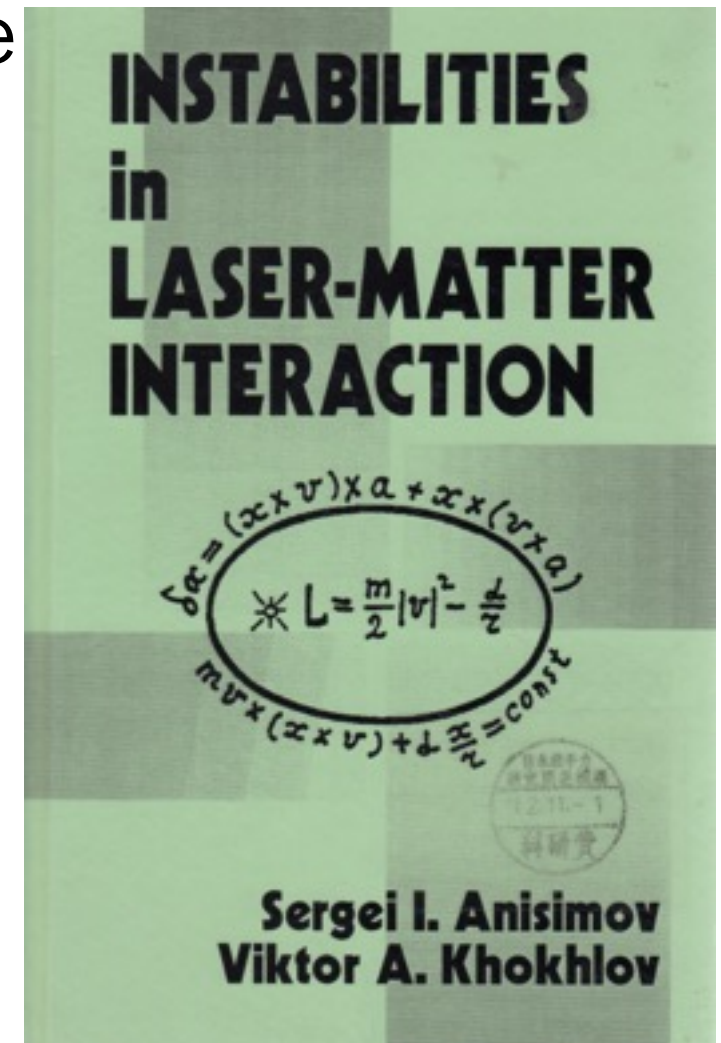


- Extensive experimental investigations have been carried out.
- Property of particles critically depends on laser irradiation.
- Observation of particles is difficult; simulation may be useful for optimization.
- Properties of particles including absorption of laser are interesting and modeling is a challenge, in the point of view of basic science.

Present status of modeling particle debris

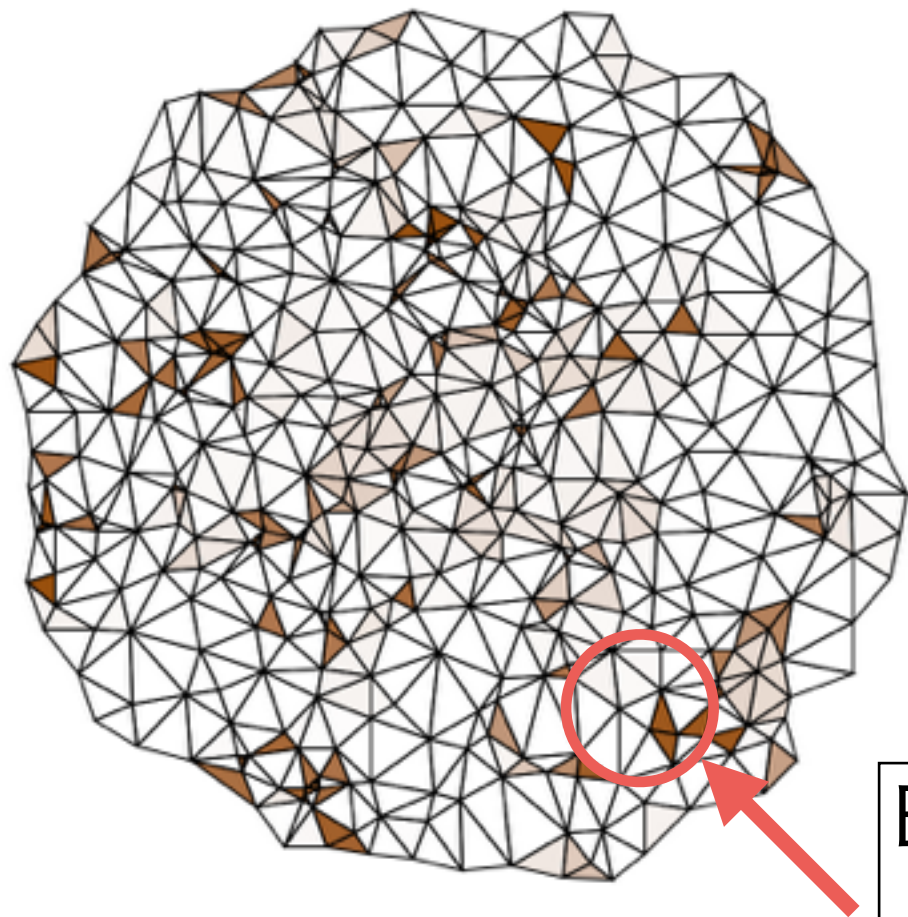
We propose Lagrangian hydrodynamics model with rezoning algorithms with which dynamics of gas bubbles in liquid and particles in gas are taken into account.

- Anisimov suggested emission of particle debris though instabilities in laser-matter interaction, did not provide methods for analysis.
- Temporal and spatial scale of MD simulation is too small.
- Present Eulerian hydrodynamics model has difficulties to take liquid-to-gas transition into account.



Concept of Lagrangian hydrodynamics model

- Lagrangian model uses mesh moves with fluid.
- We develop rezoning algorithms to place meshes along distribution of material.



Distribution of particles is scale-free, that allows analysis at an arbitrary scale. Statistics of particles rather than development of each particle is interested.

*surface tension is small if $r > 100$ nm

Even expansion is a transient phenomena, thermal equilibrium stands inside the small volume. Fraction of liquid/gas can be determined using EOS.

Basic equations

Equation of motion

$$\rho \frac{d\mathbf{u}}{dt} = -\nabla P$$

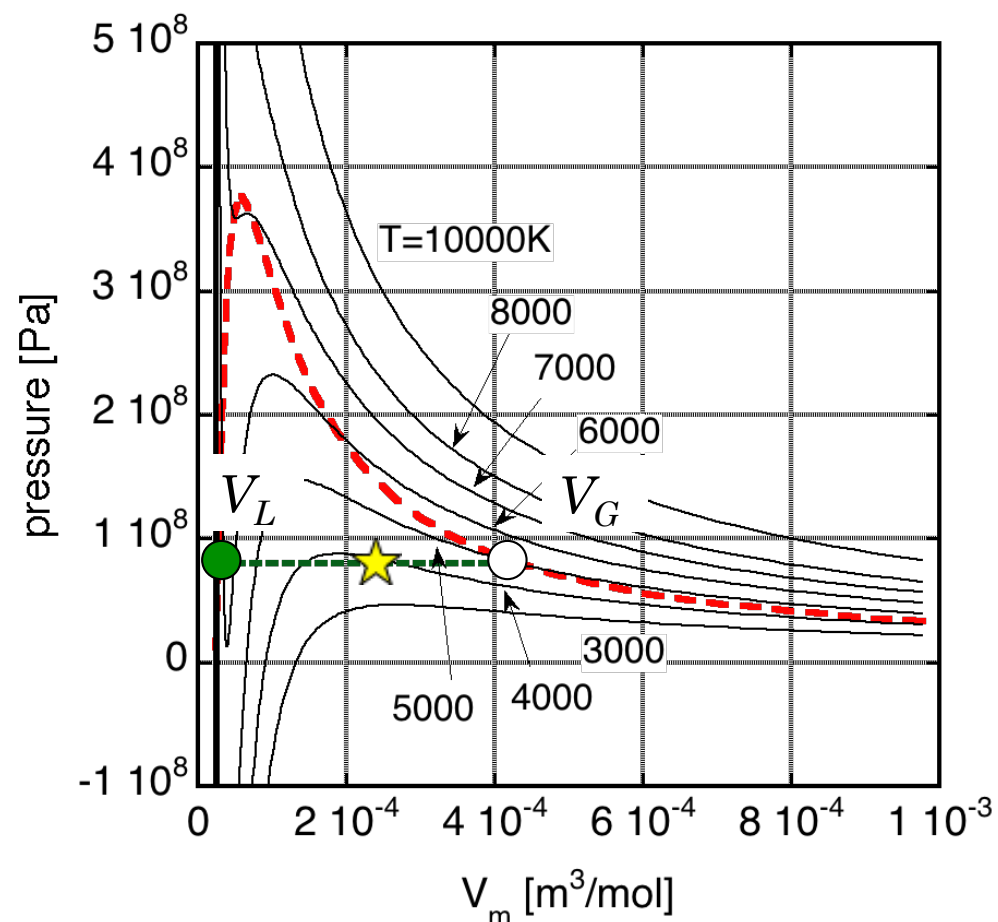
Equation of energy

$$dU_m = dQ_m - PdV_m$$

Van-der-Waals
equation of state

$$P = \frac{RT}{V_m - b} - \frac{a}{V_m^2}$$

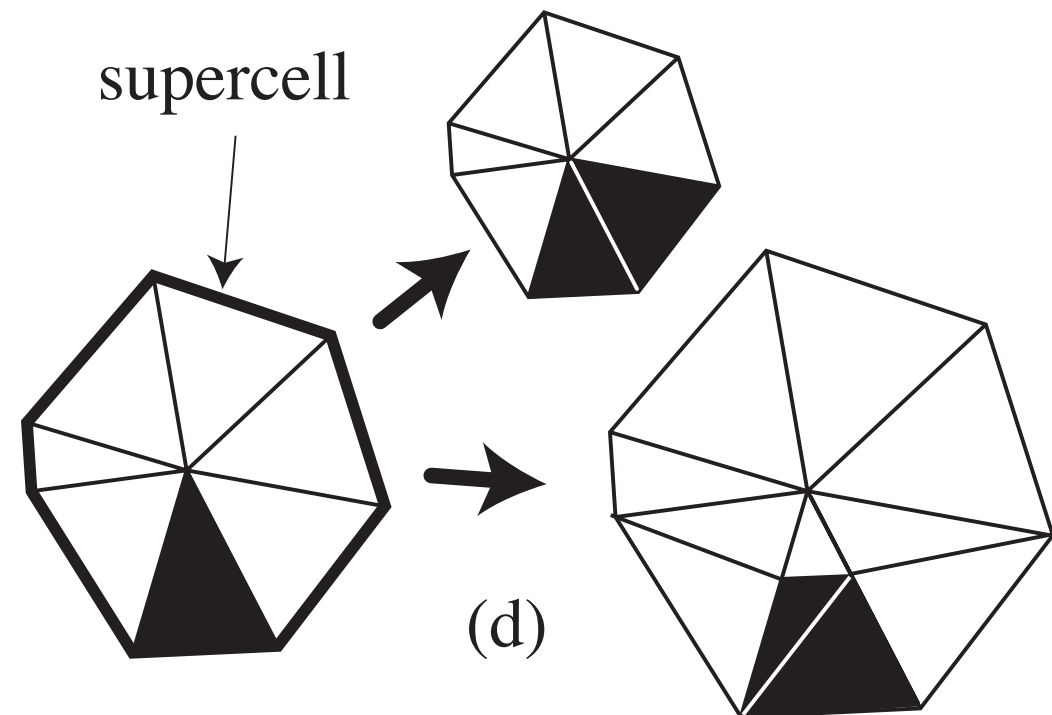
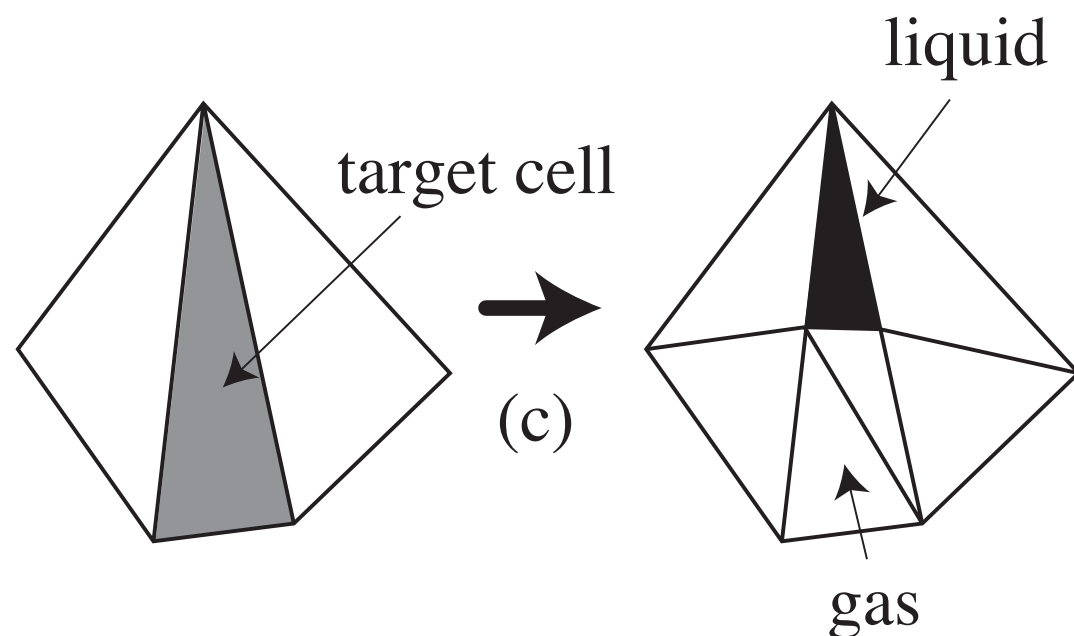
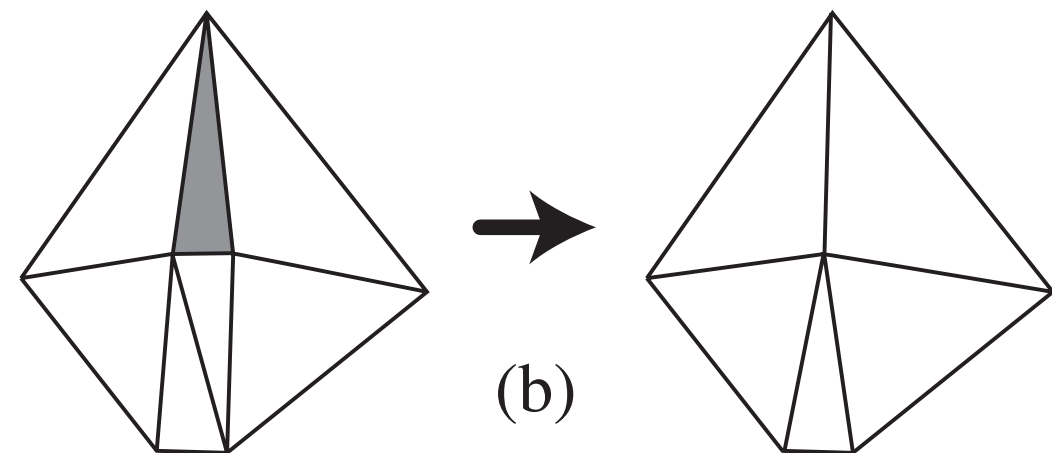
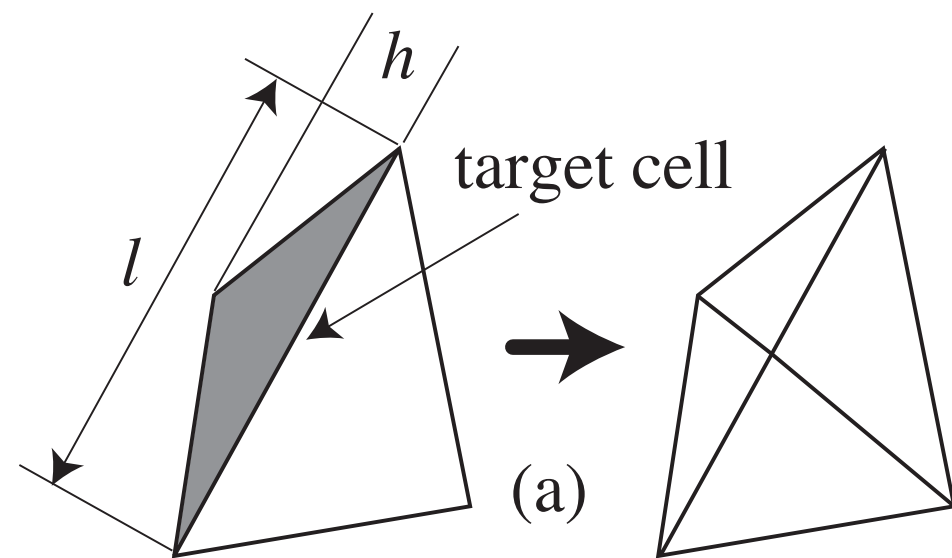
$$U_m = A_m + TS_m = \frac{3}{2}RT - \frac{a}{V_m}$$



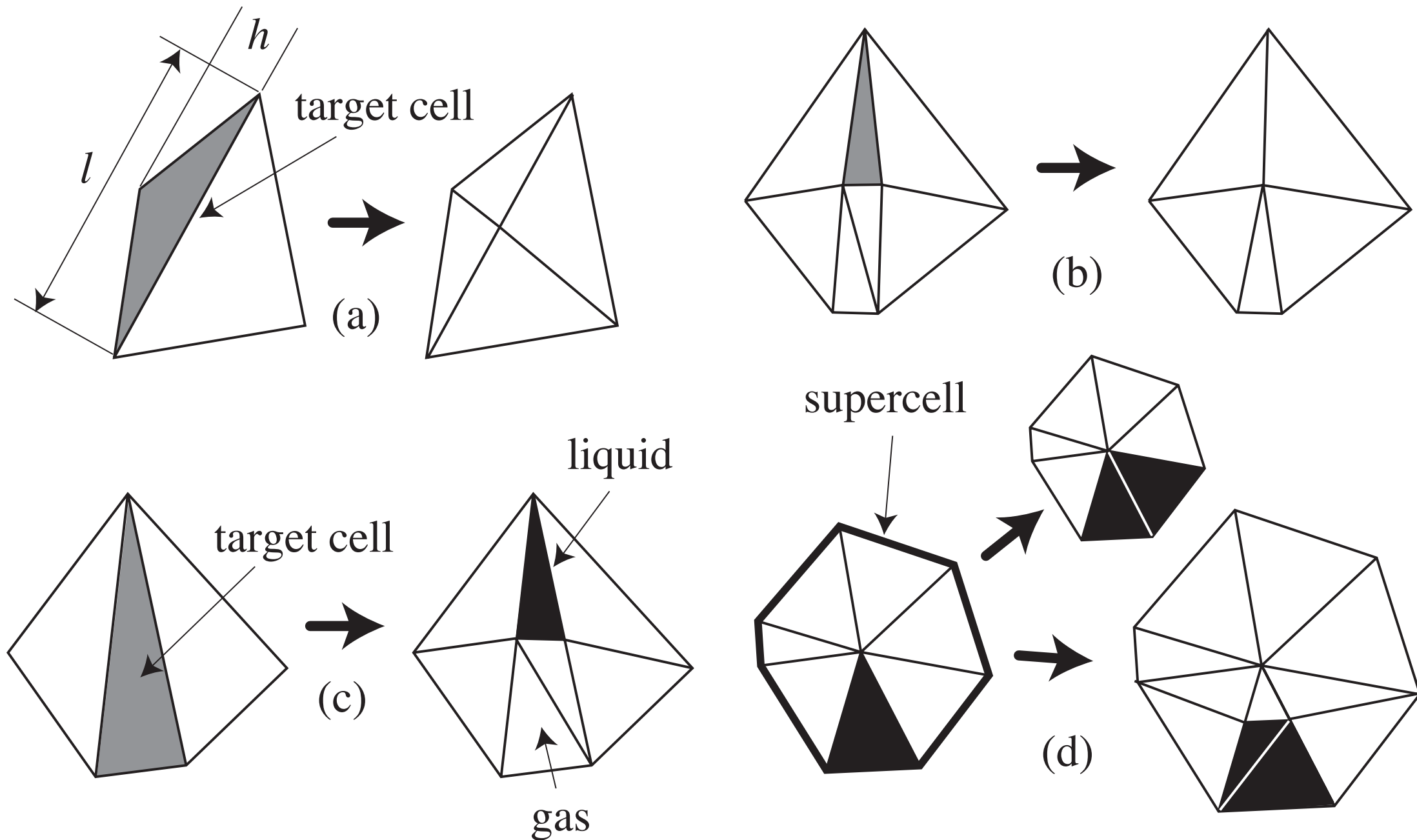
- Pressure and internal energy are given in analytical forms.
- Represents two phase condition, with ratio between liquid and gas for given temperature and density.

Rezoning algorithms

Cell is divided or united with neighboring cells to reduce distortion of the mesh, conserving mass and internal energy.



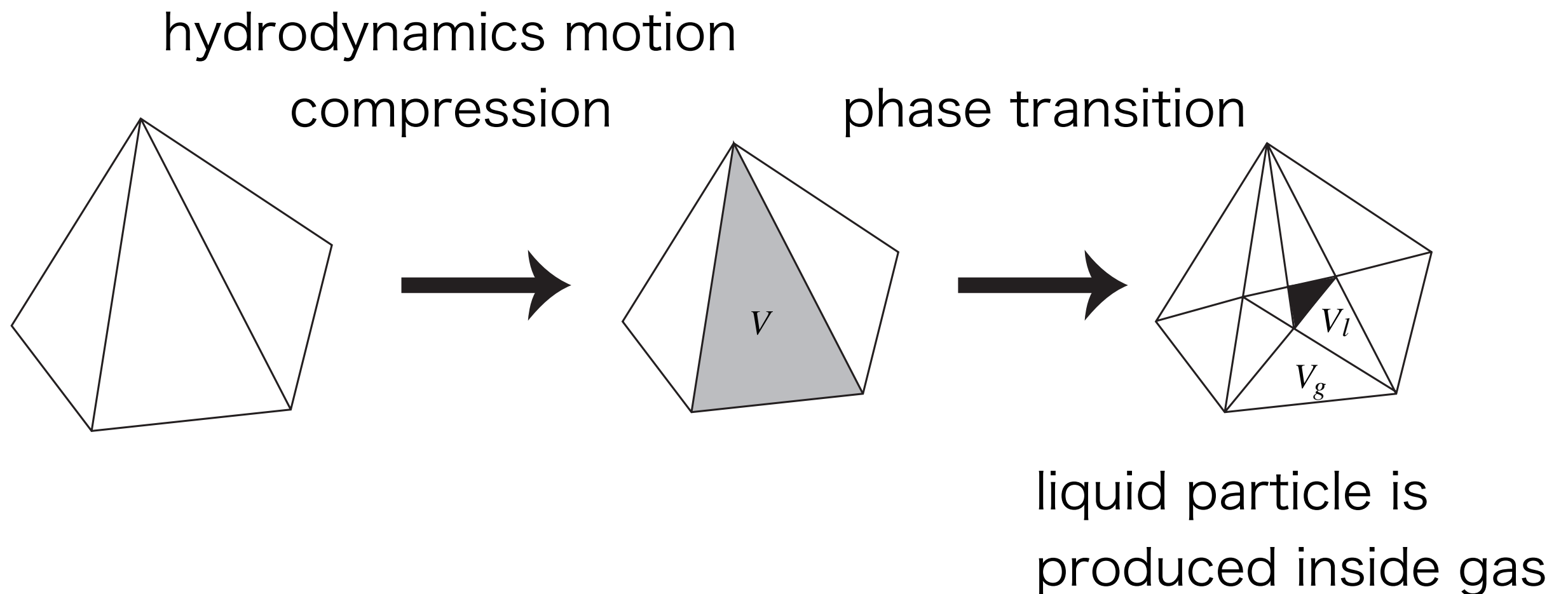
Liquid-to-gas transition algorithms



- Cell is divided to liquid and gas regions.
- Number of liquid(gas) cells in a supercell is increased to represent continuous evaporation and condensation.

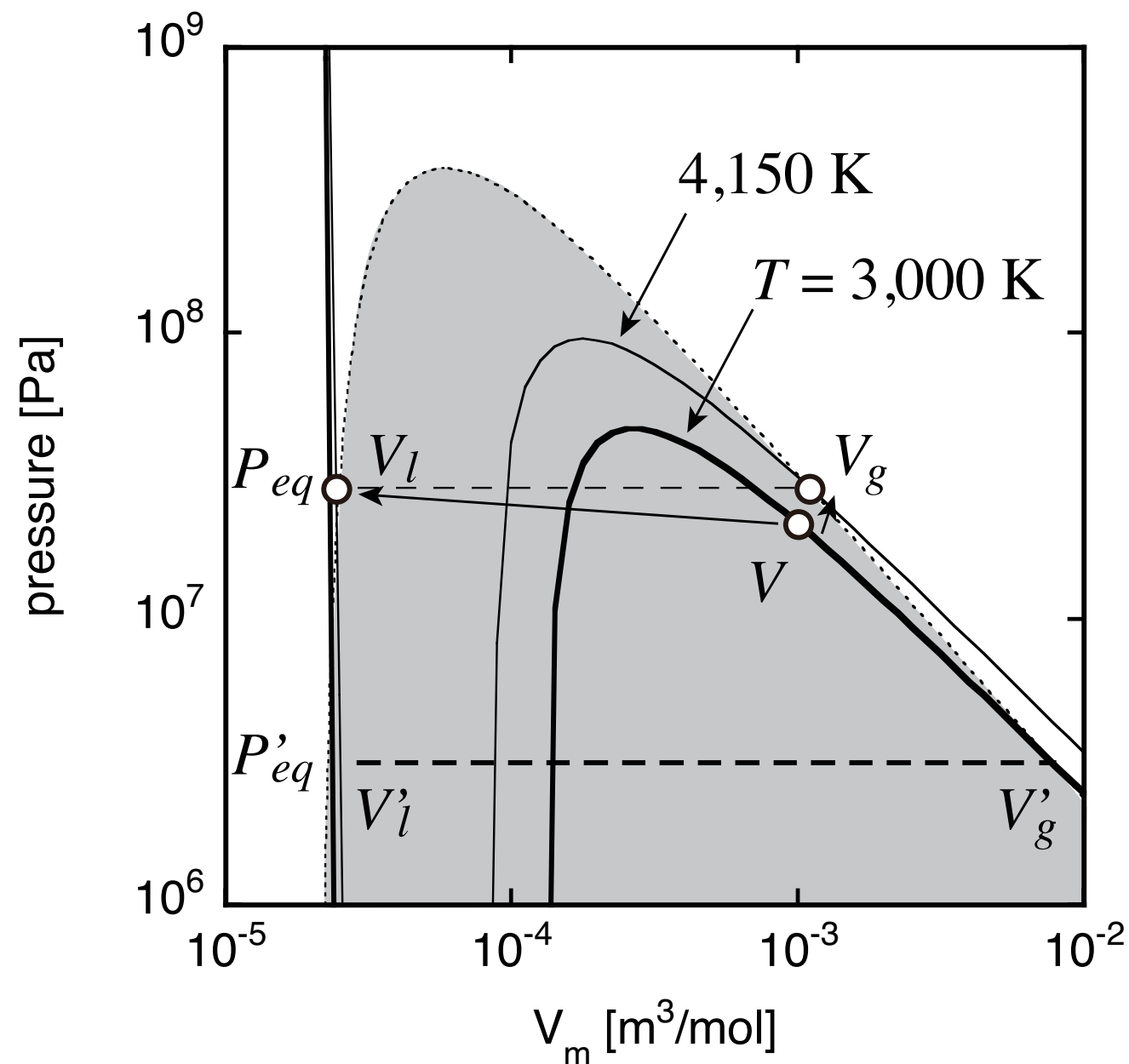
Time splitting

- Calculation of hydrodynamic and rezoning/phase-transition are carried out alternately.
- At each time step, appropriate ratio between liquid and gas of the target cell is evaluated using EOS, and the cell is divided to have liquid and gas regions.



Determination of ratio between liquid and gas

- Ratio between liquid and gas inside the cell is determined using EOS given the temperature and density of the cell.



- Difference of temperature before ($3,000 \text{ K}$) and after ($4,150 \text{ K}$) arises from difference of internal energy of liquid and gas phase, which corresponds to latent heat.

Test cases

- Calculation of low density (gas) target agrees with 1D model.
- Temporal evolution of density and temperature is calculated for tin cylinder heated uniformly and constantly; entire material is evaporated to form gas after long time.

initial diameter = 20 μm

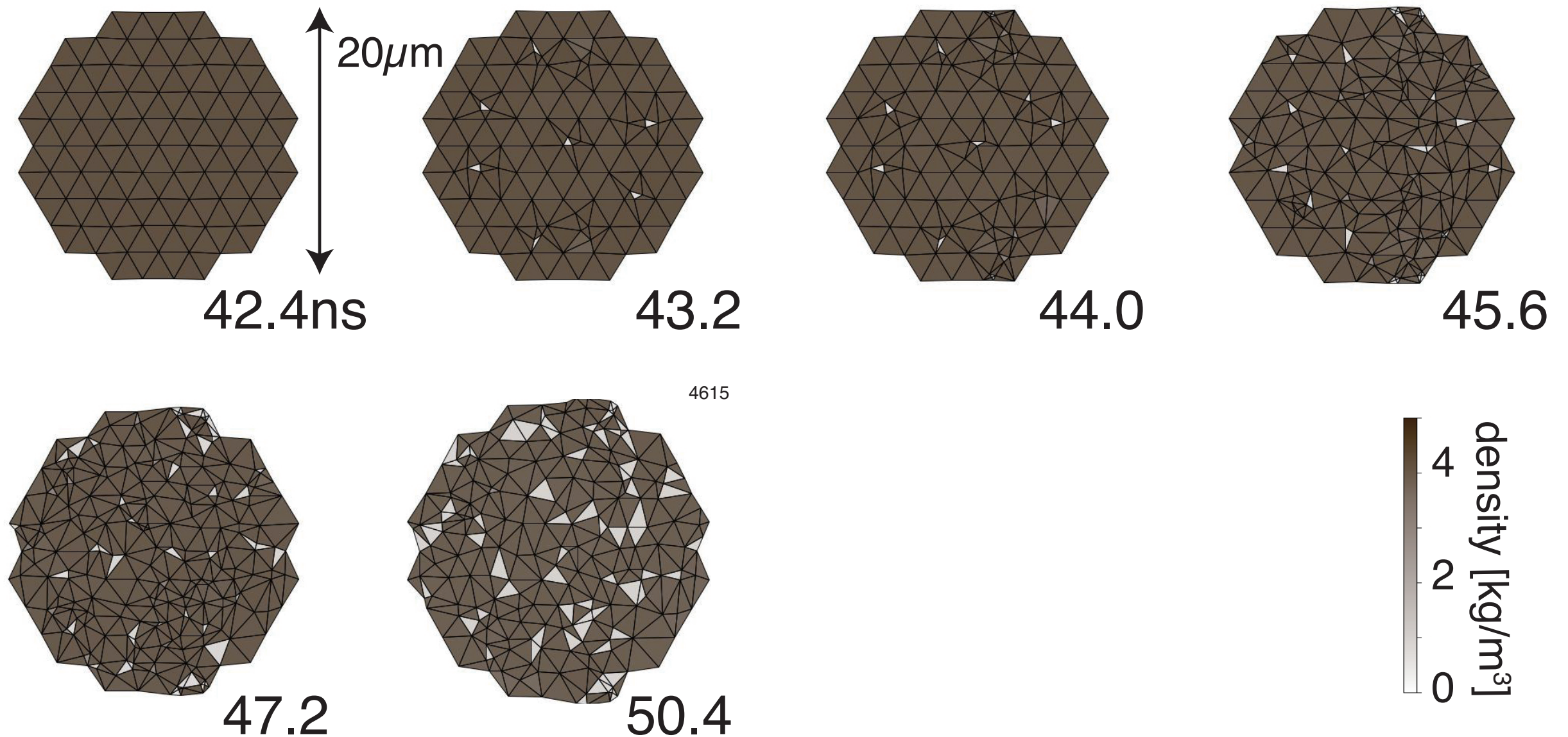
density = $5.5 \times 10^3 \text{ kg/m}^3$

temperature = 2,000 K

heating rate = $2.5 - 6 \times 10^{12} \text{ W/mol}$

Initial bubble formation

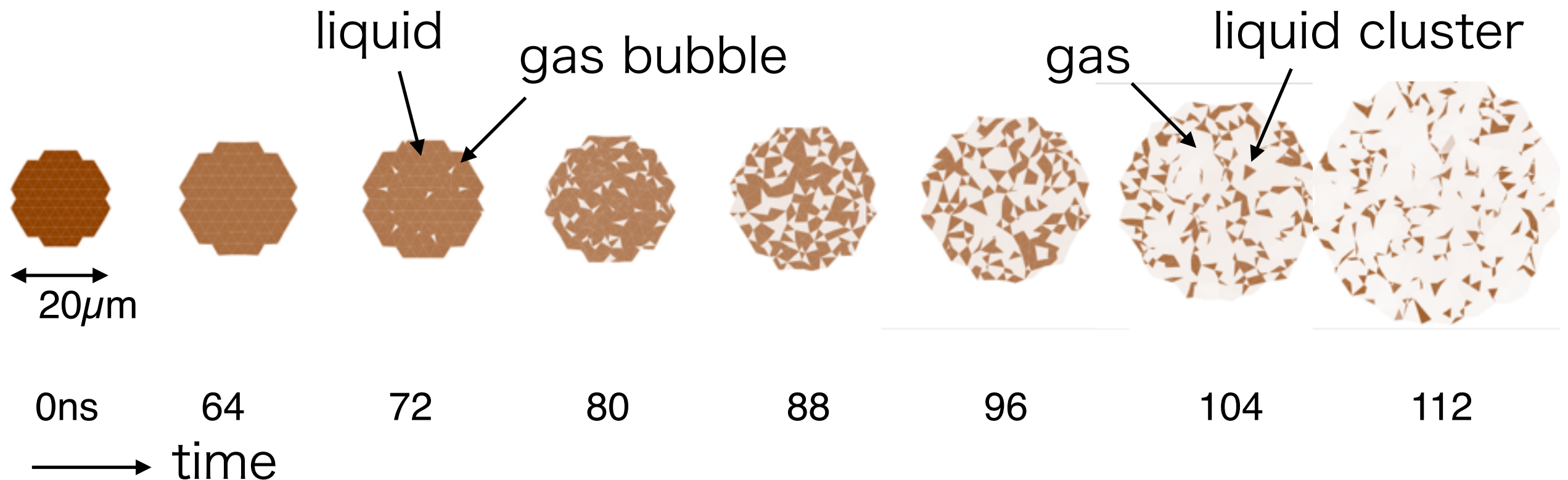
Rezoning algorithm is activated by small increase of volume to form bubbles inside the liquid target.



Result

- Bubbles appear inside the liquid target, which grow to break the target into particles.
- Target is at rest until gas phase becomes dominant, then expands rapidly.

Density profile of uniformly heated droplet



Results for different heating rates

Particle debris are emitted at low heating rates

$2.5 \times 10^{12} \text{W/mol}$



40ns

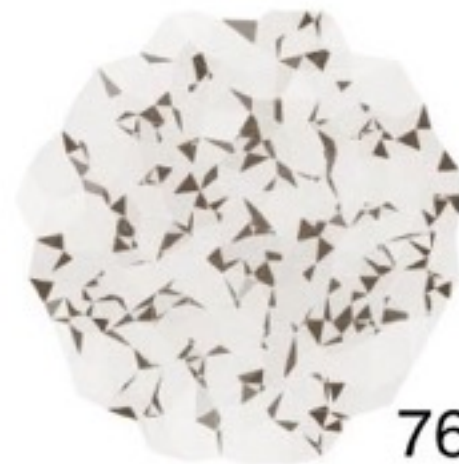
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52



64



76



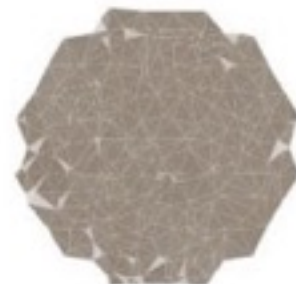
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$6 \times 10^{12} \text{W/mol}$

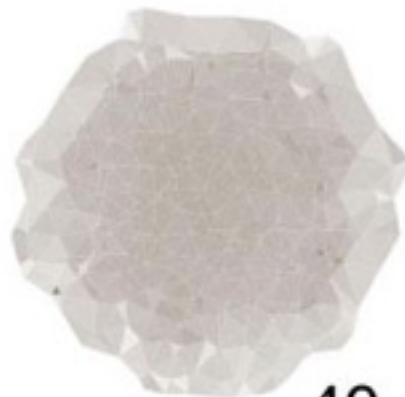


24ns

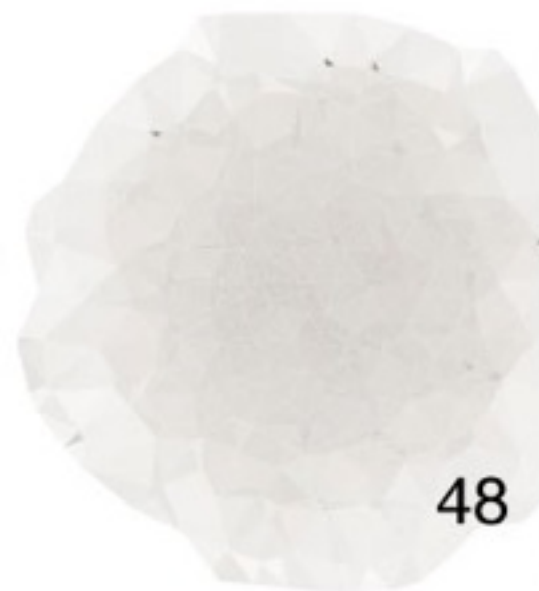
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40

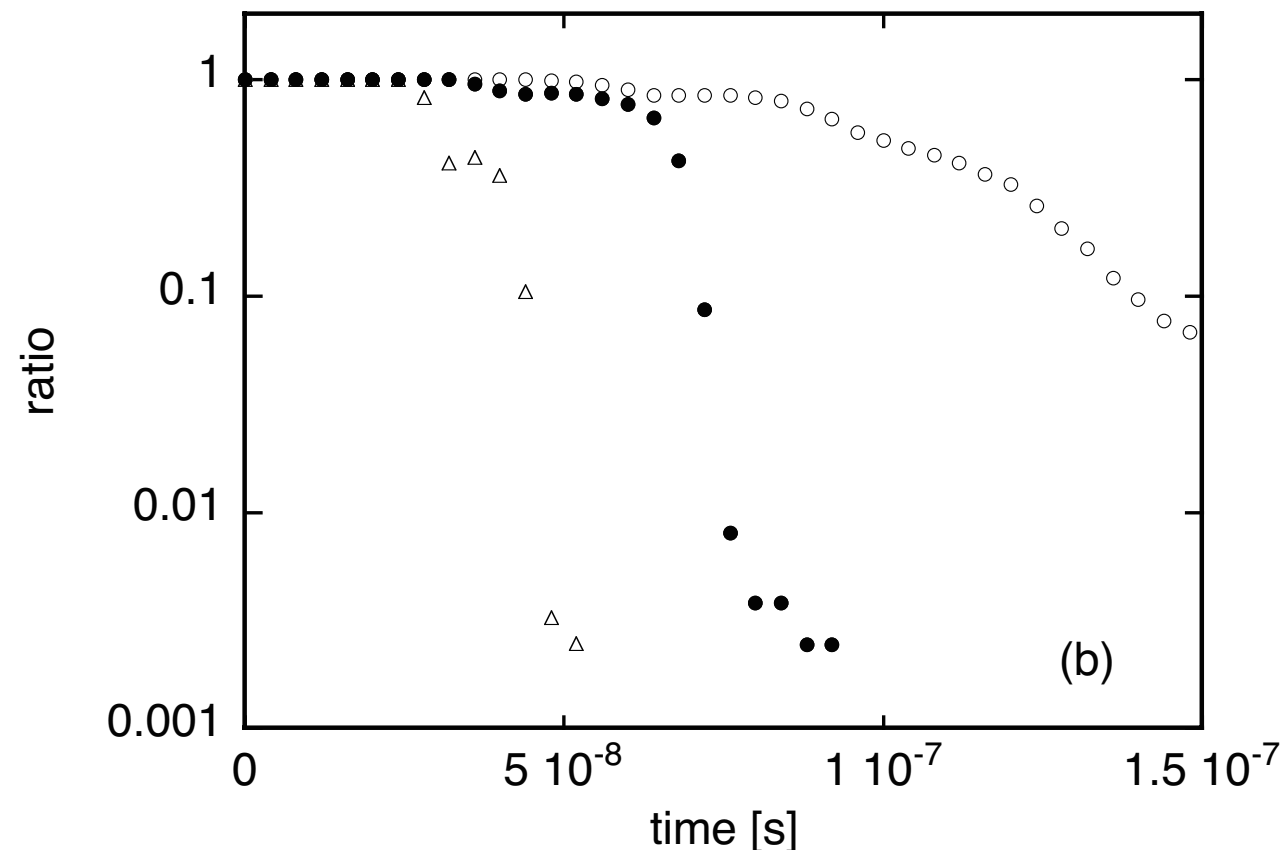
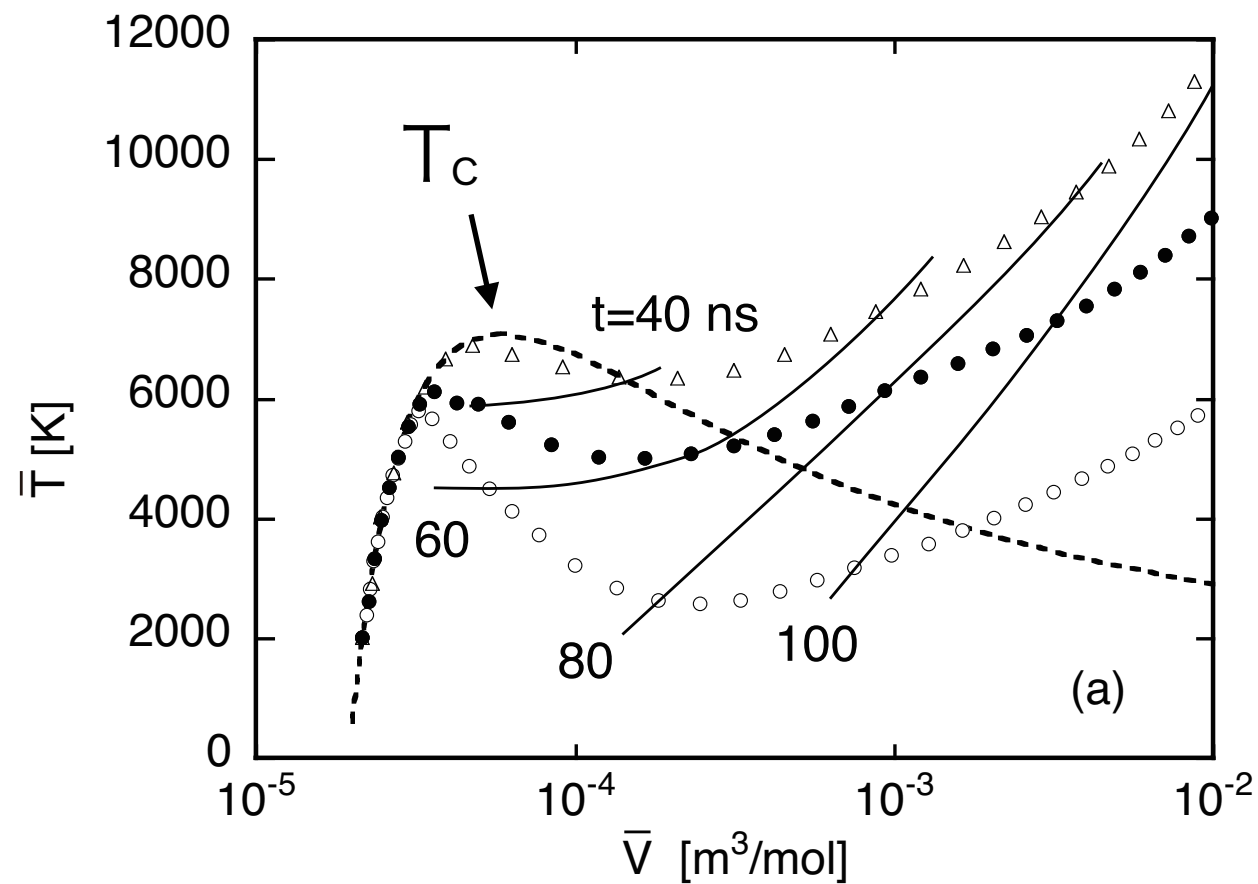


48



56

Criteria of emission of particle debris



6
4
Averaged temperature and
volume of entire target

2.5 Heating rate $\times 10^{12}$ [W/mol]

Two phase region

At small heating rates, target expands through two phase region, whereas at large heating rates, temperature immediately exceeds T_c thus particle formation does not take place.

Ratio of liquid phase

Discussion

- We investigate emission of particle debris from laser ablation of Sn droplet using hydrodynamics model with coarse grained mesh to investigate the statistical behavior of particles
- Calculations of heated Sn target show that particles are emitted at relatively low heating rates.
- Emission of particle debris from shock driven target will be investigated; algorithms to track motion of particles for a long time may be necessary.